

CLAIMS

1. A high-strength hot-rolled steel sheet
excellent in shape fixability, wherein ferrite or bainite
is the maximum phase in terms of percent volume,
5 satisfying all of the following at least at 1/2
of the sheet thickness:

(1) a mean value of X-ray random intensity
ratios of a group of $\{100\}\langle 011\rangle$ to $\{223\}\langle 110\rangle$
orientations is 2.5 or more,

10 (2) a mean value of X-ray random intensity
ratio of three orientations of $\{554\}\langle 225\rangle$, $\{111\}\langle 112\rangle$,
 $\{111\}\langle 110\rangle$ is 3.5 or less,

(3) X-ray random intensity ratio of $\{100\}\langle 011\rangle$
is larger than that of $\{211\}\langle 011\rangle$,

15 (4) X-ray random intensity ratio of $\{100\}\langle 011\rangle$
is 2.5 or more,

having at least one of an r-value in a rolling
direction and the r-value in a direction perpendicular to
the rolling direction is 0.7 or less,

20 having anisotropy of uniform elongation $\Delta uE1$
is 4% or less,

having an anisotropy of local elongation $\Delta LE1$
is 2% or more, and

having an $\Delta uE1$ which is $\Delta LE1$ or less,

25 where:

$$\Delta uE1 = \{ |uE1(L) - uE1(45^\circ)| + |uE1(C) - uE1(45^\circ)| \} / 2$$

$$\Delta LE1 = \{ |LE1(L) - LE1(45^\circ)| + |LE1(C) - LE1(45^\circ)| \} / 2$$

$uE1(L)$: Uniform elongation in a rolling direction

$uE1(C)$: Uniform elongation in a transverse direction

30 $uE1(45^\circ)$: Uniform elongation in a 45° direction

$LE1(L)$: Local elongation in a rolling direction

$LE1(C)$: Local elongation in a transverse direction

$LE1(45^\circ)$: Local elongation in a 45° direction.

2. A high-strength hot-rolled steel sheet
35 excellent in shape fixability according to claim 1,

characterized in that an occupancy rate of iron carbide, diameter of which is 0.2 μm or more, is 0.3% or less.

3. A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 1,
5 characterized in that an aging index AI is 8 MPa or more.

4. A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 1,
characterized by containing, in terms of weight %,
C: 0.01 to 0.2%,
10 Si: 0.001 to 2.5%,
Mn: 0.01 to 2.5%,
P: 0.2% or less,
S: 0.03% or less,
Al: 0.01 to 2%,
15 N: 0.01% or less, and
O: 0.01% or less

and remainder Fe and unavoidable impurities.

5. A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 4,
20 characterized by further containing at least one or more element selected from Nb, Ti and V with a total of 0.001 to 0.8%, in terms of weight %.

6. A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 4 or 5,
25 characterized by further containing at least one or more, in terms of weight %,

B: 0.01% or less,
Mo: 1% or less,
Cr: 1% or less,
30 Cu: 2% or less,
Ni: 1% or less,
Sn: 0.2% or less,
Co: 2% or less,
Ca: 0.0005 to 0.005%,
35 Rem: 0.001 to 0.05%,
Mg: 0.0001 to 0.05%,
Ta: 0.0001 to 0.05%.

7. A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 1, characterized by containing, in terms of weight %,

C: 0.02 to 0.3%,

5 at least one or more element selected from the following group consisting of, total 0.1 to 3.5%, in terms of weight %,

Mn: 0.05 to 3%,

NI: 3% or less,

10 Cr: 3% or less,

Cu: 3% or less,

Mo: 1% or less,

Co: 3% or less and

Sn: 0.2% or less,

15 at least one or both consisting of, total 0.02 to 3% in terms of weight %,

Si: 3% or less and

Al: 3% or less

20 and remainder Fe and unavoidable impurities, and having multi-phase structure, wherein ferrite or bainite is the maximum phase in terms of percent volume, and a percent volume of martensite is 1 to 25%.

8. A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 7,

25 characterized by containing, in terms of weight %, at least one or more element selected from Nb, Ti and V with a total of 0.001 to 0.8%, in terms of weight %.

9. A high-strength hot-rolled steel sheet excellent in shape fixability according to claim 7 or 8,

30 characterized by further containing at the least of one or more element selected from the following group consisting of, in terms of weight %,

P: 0.2% or less,

B: 0.01% or less,

35 Ca: 0.0005 to 0.005% and

Rem: 0.001 to 0.02%

10. A high-strength hot-rolled steel sheet

excellent in shape fixability according to claim 4 or 5,
wherein the steel sheet is plated.

11. A high-strength hot-rolled steel sheet
excellent in shape fixability according to claim 7 or 8,
5 wherein the steel sheet is plated.

12. A method of producing a high-strength hot-
rolled steel sheet excellent in shape fixability
comprising the following steps,

10 hot-rolling a cast slab having a composition
according to claim 4 or 5 as cast or cooled once, then
reheated to a temperature range of 1000-1300°C, with a
total reduction ratio of 25% or more at Ar_3 to
(Ar_3+150)°C, temperature at finishing hot-rolling start,
TFS, and temperature at finishing hot-rolling end, TFE,
15 simultaneously satisfies following Equations (1) to (4),
and

cooling hot-rolled steel sheet, then
coiling at below critical temperature T_0
determined by the chemical composition of the steel sheet
20 shown in the following Equation (5) and a temperature of
400 to 700°C,

$$TFE \geq Ar_3 \quad (1)$$

$$TFE \geq 800^\circ C \quad (1')$$

$$TFS \leq 1100^\circ C \quad (2)$$

25 $20^\circ C \leq TFS - TFE \leq 120^\circ C \quad (4)$

$$T_0 = -650.4 \times \{C\% / (1.82 \times C\% - 0.001)\} + B \quad (5)$$

where B is found from the composition of the
steel expressed by weight %

$$B = -50.6 \times Mneq + 894.3$$

30 $Mneq = Mn\% + 0.24 \times Ni\% + 0.13 \times Si\% + 0.38 \times Mo\% + 0.55 \times Cr\%$
 $+ 0.16 \times Cu\% - 0.50 \times Al\% - 0.45 \times Co\% + 0.90 \times V\%$

$$Ar_3 = 901 - 325 \times C\% + 33 \times Si\% + 287 \times P\% + 40 \times Al\%$$

$$- 92 \times (Mn\% + Mo\% + Cu\%)$$

$$- 46 \times (Cr\% + Ni\%)$$

13. A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability according to claim 12, characterized by further controlling a friction coefficient to not more than 0.2 in at least one pass in the hot-rolling in a temperature range of Ar_3 to $(Ar_3+150)^\circ C$.

14. A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability characterized by applying skin pass rolling of 0.1 to 5% to hot-rolled steel sheet produced by the method of producing a high-strength hot-rolled steel sheet excellent in shape fixability according to claim 12.

15. A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability comprising the following steps,

hot-rolling a cast slab having a composition according to claim 7 or 8 as cast or cooled once, then reheated to a range of 1000 to 1300 $^\circ C$, with a total reduction ratios of 25% or more at Ar_3 to $(Ar_3+150)^\circ C$, temperature at finishing hot-rolling start, TFS, and temperature at finishing hot-rolling end, TFE, and calculated residual strain $\Delta\epsilon$ to simultaneously satisfy following relations (1) to (4), and

cooling hot-rolled steel sheet, then coiling at below critical temperature T_0 determined by the chemical composition of the steel shown in the following relation (5) and a temperature of not more than 400 $^\circ C$:

$$TFE \geq Ar_3 (^\circ C) \quad (1)$$

$$TFS \leq 1100^\circ C \quad (2)$$

$$\Delta\epsilon \geq (TFS - TFE) / 375 \quad (3)$$

$$20^\circ C \leq (TFS - TFE) \leq 120^\circ C \quad (4)$$

$$T_0 = -650.4 \times \{C\% / (1.82 \times C\% - 0.001)\} + B \quad (5)$$

where, B is found from the composition of the steel expressed by weight%,

$$B = -50.6 \times \text{Mneq} + 894.3$$

$$\text{Mneq} = \text{Mn}\% + 0.24 \times \text{Ni}\% + 0.13 \times \text{Si}\% + 0.38 \times \text{Mo}\% + 0.55 \times \text{Cr}\% \\ + 0.16 \times \text{Cu}\% - 0.50 \times \text{Al}\% - 0.45 \times \text{Co}\% + 0.90 \times \text{V}\%$$

where,

5
$$\text{Ar}_3 = 901 - 325 \times \text{C}\% + 33 \times \text{Si}\% + 287 \times \text{P}\% + 40 \times \text{Al}\% - 92 \\ \times (\text{Mn}\% + \text{Mo}\% + \text{Cu}\%) - 46 \times (\text{Cr}\% + \text{Ni}\%)$$

10 $\Delta\epsilon$ is found from the equivalent strain ϵ_i (i is 1 to n) given at each stand of the n stages of finishing rolling for the rolling, time t_i (sec) ($i=1$ to $n-1$) between stands, time t_n (sec) from the final stand to the start of cooling, rolling temperature T_i (K) ($i=1$ to n) at each stand, and a constant $R=1.987$.

$$\epsilon = \Delta\epsilon_1 + \Delta\epsilon_2 + \dots + \Delta\epsilon_n$$

$$\text{where, } \Delta\epsilon_i = \epsilon_i \times \exp\{-(t_i^*/\tau_n)^{2/3}\}$$

15
$$\tau_n = 8.46 \times 10^{-9} \times \exp\{43800/R/T_i\}$$

$$t_i^* = \tau_n \times (t_i/\tau_i + t(i+1)/\tau(i+1) + \dots + t_n/\tau_n)$$

16. A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability according to claim 15, characterized by further
20 controlling a friction coefficient to not more than 0.2 in at least one pass in the hot-rolling in a temperature range of Ar_3 to $(\text{Ar}_3 + 150)^\circ\text{C}$.

17. A method of producing a high-strength hot-rolled steel sheet excellent in shape fixability
25 characterized by applying skin pass rolling of 0.1 to 5% to hot-rolled steel sheet produced by the method of producing a high-strength hot-rolled steel sheet excellent in shape fixability according to claim 15.